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# THE VARIATION OF THE SALT CONCENTRATION AT THE DISCHARGE OF A RIVER INTO A SALINE WATER

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## Abstract

A plume model is used to describe the variation of the salt concentration at the discharge of a river into a saline water. The integral model of the plume behavior consists of a set of ordinary differential equations derived from conservation of mass, momentum and salt concentration. The temperatures of the plume and ambient saline water are considered equal. The concentration of the salt in the river water is null. The saline water is assumed motionless. After release from the river, the concentration of the salt in the plume increases by mixing with the ambient saline water. The rate of mixing depends upon the local plume and ambient fluid properties such as velocity and salt concentration.

## 1 Introduction

River inflows and their associated buoyant plumes are a major source of nutrients, sediments and contaminants to coastal waters. Also, they are a major threat to coastal and marine ecosystems such as coral reefs and seagrass beds. The plume, which is characterized by low-salinity water from the river, can determine the water density structure and circulation systems for these regions. For these reasons, considerable effort has been made to monitor the circulation within river plumes in order to determine the transport and dispersal of river-borne matter in the coastal zone (see for example, [7], [11], [18], [24] and

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[25]). Sea surface salinity in coastal oceans is a direct indicator of riverine plumes and provides essential information about the ocean environment and ecosystem. For the freshwater plumes produced by river discharges buoyancy often leads to expansion primarily along the surface. The freshwater impact on salinity is mostly noted through density currents in the sea surface. River plumes exhibit a great variety of spatial scales and shapes. Based on the values of the Kelvin number,  $R_K$ , Garvine [12] sizes the river plumes into: (1) small-scale plumes and (2) large-scale plumes. The Kelvin number,  $R_K$ , is defined as,

$$R_K = \frac{fw_0}{\sqrt{b_0h_0}} \quad (1)$$

where  $f$  is the local Coriolis parameter (frequency),  $w_0$  the river width,  $h_0$  the upper layer thickness,  $b_0 = g(\rho_a - \rho_p)/\rho_a$ ,  $\rho_a$  the ambient density,  $\rho_p$  the buoyant fluid density and  $g$  the gravity acceleration. For small scale plumes ( $R_K < 1$ ) the inertial effects are more important than earths rotation. For large scale plumes ( $R_K \geq 1$ ) the effect of earths rotation becomes important. From another point of view, the river plumes are grouped as, [4]: (i) surface trapped or (ii) bottom attached. For the surface trapped plumes the fresh water forms a shallow, surface trapped layer that spreads over the ambient shelf water and exhibits strong vertical stratification. For the bottom attached plumes a significant portion of the plume spans the water column from surface to bottom.

There is not a single, unitary class of mathematical models that describe the river plumes behavior. Chatanantavet and Lamb [5] and Poggioli [22] developed a 1-D mathematical model based on the hydraulics of the open channel. Considering the ocean barotropic, inviscid, uniformly rotating, the 2-D inviscid barotropic vorticity equation was used in [13], [16], [17], [19], [25], and [26]. The semi-spectral 3-D primitive equation model proposed by Haidvogel et al. [14] was used and improved in [3], [9], [10], [21], [27]. Osadchiev and Zavialov [20] proposed a Lagrange mathematical model based on tracking and dissipation of imaginary individual particles of the river water discharged into the sea. Laboratory experiments used to simulate the plume behavior can be viewed in [15], [22].

The aim of the present paper is to describe the discharge of a river into a saline water using an integral plume model. The integral plume model was used to simulate the deep-sea gravity currents [1], melting of the glacial system [2], hydrothermal vents from fracture area at the sea floor, [6] and deep waters oil blowout plumes, [8]. This paper is organized as follows. Section 2 describes the integral plume model used in this work. The numerical solving of the present mathematical model is briefly presented in Sect. 3. The numerical experiments made and the results obtained are presented in Sect. 4. Finally,

some concluding remarks are briefly mentioned in Sect. 5.

## 2 Model equations

Generally, it is assumed that marine plumes exhibit similar behaviour to aerial plumes. However, marine plumes show similar characteristics to aerial plumes only qualitatively. Quantitatively, they are different. The evolution of marine plumes is influenced significantly by a large number of factors, such as the bathymetry, the Coriolis force, the river discharge, winds, tides and other coastal processes. The case analysed in the present work describes the discharge of a river into a salt lake. Thus, from the beginning one can consider that the present plume is a surface trapped, small scale one. The temperatures of the river water and the saline water are the same. The effects of the winds and saline water internal currents are neglected. Tides do not occur in the present physical environment. The saline water is considered motionless. For a latitude of approximately  $45^\circ$ , the Coriolis frequency is equal to  $f = 10^{-4} s^{-1}$ . The reduced gravitational acceleration  $b_0$  is on the order of,  $b_0 \approx 0.1 m s^{-2}$ . The values of  $h_0$  and  $w_0$  used in this work are:  $h_0 = 0.5 m \div 1 m$  and  $w_0 = 50 m$ . Under these conditions, the values of the Kelvin number are:  $R_K < 0.022$ . For these Kelvin number values the effect of earth rotation is negligible.

The plume moves in the  $y$  direction (figure 1). Under the scenario previously outlined, the following balance equations were obtained by averaging over a cross-section of the plume with area  $A = wh$  ( $w$  and  $h$  are respectively the width and height of the plume - see figures 1 and 2):

- Mass conservation

$$\frac{d}{dy} (\rho_p w h U) = \rho_a (w + 2h) V_e \quad (2)$$

- Momentum conservation

$$\frac{d}{dy} (\rho_p w h U^2) = -C_D \rho_p U^2 \rho_a (w + 2h) \quad (3)$$

- Salt conservation

$$\frac{d}{dy} (\rho_p w h U S_p) = \rho_a V_e (w + 2h) S_a \quad (4)$$

where  $C_D$  is the drag coefficient,  $S$  is the concentration of the salt,  $U$  is the average plume velocity,  $V_e$  is the entrainment (mixing) velocity of the saline

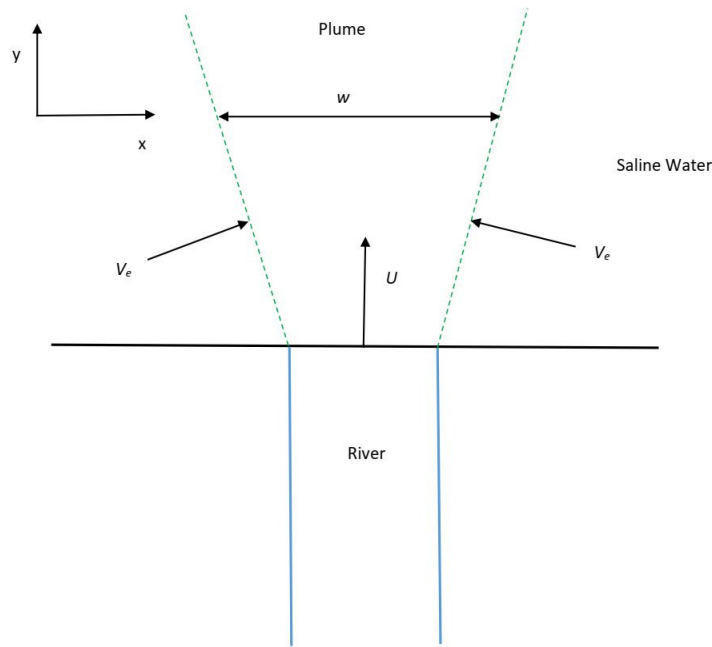


Figure 1: Plume moves in the  $y$  direction.

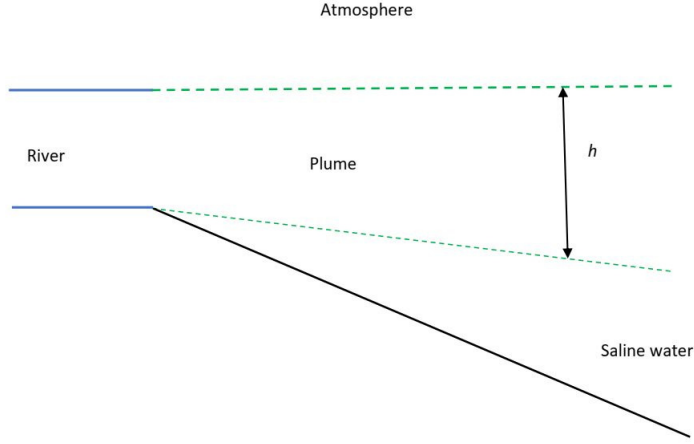


Figure 2: Plume area.

water into the plume, and  $\rho$  is the density. The subscripts  $a$  and  $p$  refer to the ambient saline water and plume, respectively. The entrainment surface into the plume is  $(w + 2h)$ . The entrainment velocity  $V_e$  was calculated with the well-known semi-empirical relation, [1],[6]:

$$V_e = \alpha U. \quad (5)$$

We have also assumed the followings:

- Constant width over thickness ratio,[1],

$$\frac{w}{h} = k = constant \gg 1 \quad (6)$$

- The density of the plume and saline water are constant and approximately equal,

$$\rho_a \approx \rho_p \quad (7)$$

For the scenario previously mentioned, after some algebraic manipulations, the mathematical model reads as:

$$\frac{dw}{dy} = \frac{k \left(1 + \frac{2}{k}\right)}{2U} (2V_e + C_D U) \quad (8)$$

$$\frac{dU}{dy} = -\frac{k\left(1 + \frac{2}{k}\right)}{w}(C_D U + V_e) \quad (9)$$

$$\frac{dS_p}{dy} = \frac{k\left(1 + \frac{2}{k}\right)}{wU} V_e (S_a - S_p) \quad (10)$$

with the initial conditions :

$$y = 0, w = w_0, U = U_0, S_p = 0. \quad (11)$$

### 3 Method of solution

The mathematical model equations (4 -6) with the initial conditions (7) were solved numerically. The MATLAB routine ode45 was used (the present problem is not a stiff system of ordinary differential equations). The error tolerance considered was  $10^{-6}$ . Different values were considered for the final  $y$  values such that the integration was stopped when,

$$U \leq 0.005m/sec. \quad (12)$$

### 4 Results

The parameters of the present mathematical model are:  $C_D$ ,  $S_a$ ,  $a$  and  $k$ . According to [1], the value recommended for  $C_D$  is:  $C_D = 0.013$ . Usually, the value of  $a$  is determined experimentally. The value of this parameter remains a matter for debate. However, commonly accepted values vary from  $a = 0.054$  for jets to  $a = 0.083$  for plumes, [6]. These values represent in fact a parameterization of the turbulence. In this work the value used for  $a$  is:  $a = 0.083$ . In all numerical experiments a single value was assumed for  $S_a$ , i.e.  $S_a = 1.0$ . The geometric parameter  $k$  takes values in the range,  $k = 50 \dots 100$ . The numerical simulations were made for the following values of  $U_0$  and  $w_0$ :

$$U_0 = 0.1, 0.5, 1, 2, 5, 10m/sec, w_0 = 50m.$$

Replacing in equation (8) the expression for the entrainment velocity  $V_e$  from (5), e.g.  $V_e = \alpha U$ , one obtains, after some elementary algebraic manipulations,

$$\frac{dw}{dy} = k \left(1 + \frac{2}{k}\right) \left(\alpha + \frac{C_D}{2}\right) \quad (13)$$

Thus, the average plume velocity does not influence the width of the plume. For this reason, in figure 3, only a single curve is plotted. Figure 3 shows, according to the previous relation, that the variation of  $w$  versus  $y$  is linear and

$w$  increases with the increase in  $y$ . Applying the same algebraic manipulations, equation (10) reads as:

$$\frac{dS_p}{dy} = \frac{k \left(1 + \frac{2}{k}\right)}{w} \alpha (S_\alpha - S_p). \quad (14)$$

The previous relation shows that the salinity of the plume  $S_p$  does not depend on the initial value of the plume average velocity. The increase in the plume average velocity increases the entrainment velocity and implicitly the turbulent mixing. Figure 4 shows that the variation of  $S_p$  versus  $y$  is different compared to the variation of the plume width  $w$  versus  $y$ . The salinity of the plume increases faster with the increase in  $y$  and reaches the value of ambient salinity for low values of  $y$ . The concentration gradient between the plume and the saline water decreases significantly with the increase in  $w$ . For values of  $w$  greater than 500 it becomes smaller than 0.01. For this reason, in figure 4, the maximum value of  $y$  is smaller than the value considered in figures 3 and 5. The average plume velocity depends on the discharge rate. The increase in  $U_0$  increases the values of  $U$  (see figure 5). In figure 5 the maximum value selected for  $y$  is  $y = 15000m$  (the same value as in figure 3). We made this selection to avoid the situation of three figures with three different abscissae. Figure 5 shows that the plume length increases with the increase in  $U_0$  but, as previously mentioned, its composition remains practically the same. In all the test cases the value of  $k$  for a constant width over thickness ratio is taken to be  $k = 50$ .

## 5 Conclusions

The variation of the salt concentration at the discharge of a river into a saline water was analysed using an integral the plume model. The temperatures of the plume and ambient saline water are considered equal. The concentration of the salt in the river water is null. The saline water is assumed motionless. The main issue investigated in the present paper is the influence of the river discharge rate on the plume composition and dimensions. The results provided by the present model and presented in the previous section show that the plume salinity and width do not depend on the discharge rate. The discharge rate influences only the plume length.

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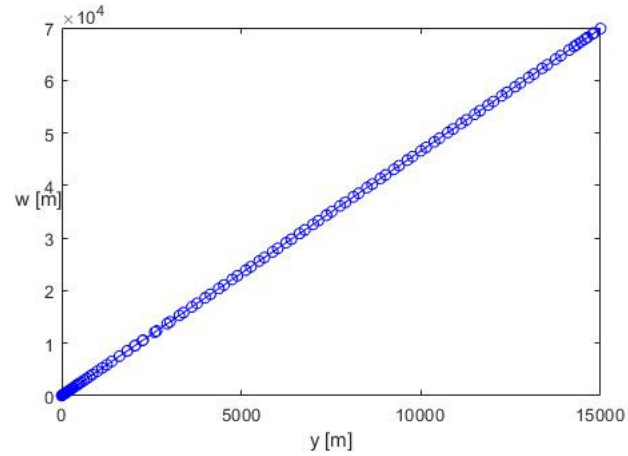


Figure 3: The variation of the plume width ( $w$ ) in the  $y$  direction ( $k = 50$ ).

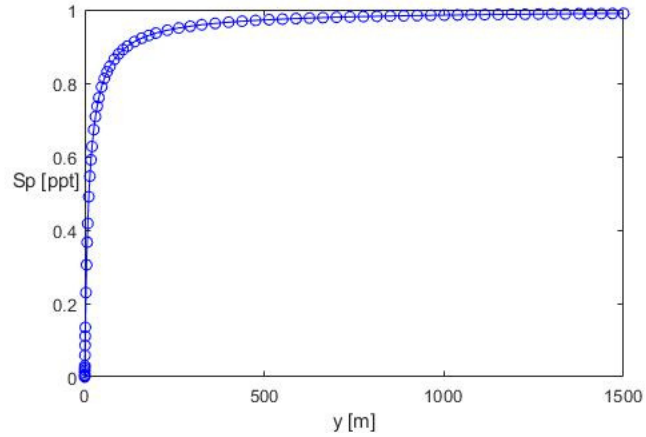


Figure 4: The variation of the salt concentration ( $S_p$ ) in the  $y$  direction, in the plume ( $k = 50$ ).



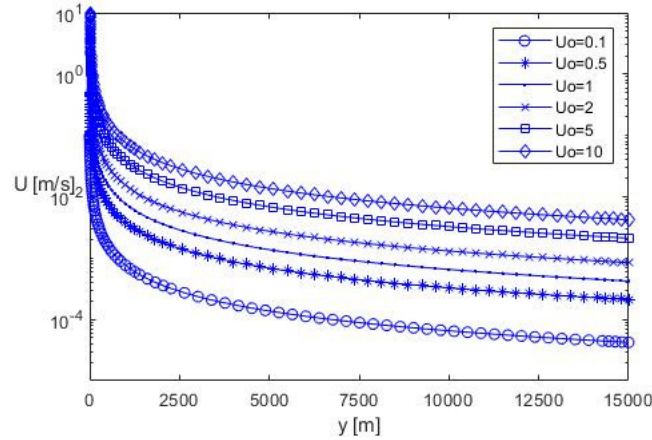


Figure 5: The variation of the average plume velocity ( $U$ ) in the  $y$  direction for different values of  $U_0$  ( $k = 50$ ).

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